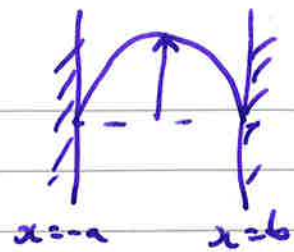


(a) Sech fully developed flow $u = w(x)\hat{z}$



$\nabla \cdot \underline{u} = 0$ (automatically)

$\rho \frac{\partial u}{\partial t} = -\nabla p + \mu \nabla^2 \underline{u} + \rho \underline{g}$ reduces to $\mu \frac{d^2 w}{dx^2} = -G + \rho g$

Integrate subject to no slip at $x = -a$ and $x = a$. $w(-a) = w(a) = 0$.

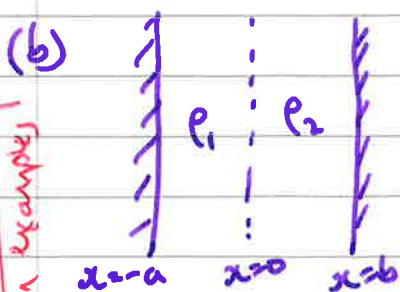
$w = \frac{(\rho g - G)}{2\mu} (x^2 + Ax + B)$ A and B to be determined.

$w(-a) = 0 \Rightarrow a^2 - Aa + B = 0 \Rightarrow a^2 - b^2 = A(a+b)$

$w(b) = 0 \Rightarrow b^2 + Ab + B = 0 \Rightarrow A = a-b, B = -ab$

Here $w = \frac{\rho g - G}{2\mu} (x^2 + (a-b)x - ab) = \frac{\rho g - G}{2\mu} (x+a)(x-b)$

Value flux per unit width $= \int_{-a}^b w dx = \int_0^{a+b} w(s) ds$ ($s = x+a$)
 $= \int_0^{a+b} \frac{\rho g - G}{2\mu} s(s-a-b) ds$
 $= \frac{(G - \rho g)}{12\mu} (a+b)^3$



$-a < x < 0 : \mu \frac{d^2 w_1}{dx^2} = -G + \rho g = \frac{(\rho_1 - \rho_2)g}{2} - \lambda \mu$

$0 < x < b : \mu \frac{d^2 w_2}{dx^2} = -G + \rho g = \frac{(\rho_2 - \rho_1)g}{2} - \lambda \mu$

Define $m = \frac{(\rho_2 - \rho_1)g}{2\mu}$

So, $\frac{d^2 w_1}{dx^2} = -m - \lambda$ and $\frac{d^2 w_2}{dx^2} = m - \lambda$

Integrating $w_1 = -\frac{(m+\lambda)}{2} x^2 + Ax + B$ } A, B, C, D to be determined.
 $w_2 = \frac{(m-\lambda)}{2} x^2 + Cx + D$

Unseen, though two fluid problems in examples

Standard calculation (Result in vectors)

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No slip $w_1(-a) = 0 \Rightarrow -(m+\lambda)\frac{a^2}{2} - Aa + B$
 $w_2(b) = 0 = (m-\lambda)\frac{b^2}{2} + Cb + D$

Interfacial conditions: $[w]_{x=0^+}^{x=0^-} = 0 \Rightarrow B = D$
 $\left[\frac{dw}{dx}\right]_{x=0^+}^{x=0^-} = 0 \Rightarrow A = C$

Then $-\frac{1}{2}(m+\lambda)a^2 - Aa - \frac{1}{2}(m-\lambda)b^2 - Cb = 0$

$\Rightarrow A = C = \frac{\lambda(b^2 - a^2) - m(a^2 + b^2)}{2(a+b)}$

or $D = B = (m+\lambda)\frac{a^2}{2} + a \cdot \frac{\lambda(b^2 - a^2) - m(a^2 + b^2)}{2(a+b)}$
 $= \frac{\lambda(a^2b + ab^2) + m(a^2b - ab^2)}{2(a+b)}$
 $= \frac{ab}{2(a+b)} (\lambda(a+b) + m(a-b))$

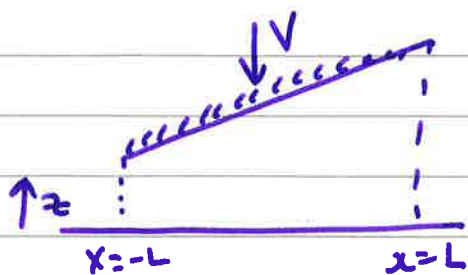
(c) Total flux $= \int_{-a}^0 w_1 dx + \int_0^b w_2 dx$
 $= \int_{-a}^0 \frac{m+\lambda}{2} x^2 dx - \int_{-a}^0 \frac{m+\lambda}{2} x^2 dx - \lambda \int_{-a}^0 \frac{x^2}{2} dx + A \int_{-a}^0 x dx + B \int_{-a}^0 dx$
 $= \frac{m}{6} (b^3 - a^3) - \frac{\lambda}{6} (b^3 + a^3) + \frac{A}{2} (b^2 - a^2) + B(a+b)$
 $= \frac{m}{6} (b^3 - a^3) - \frac{\lambda}{6} (b^3 + a^3) + \frac{(b-a)}{4} (\lambda(b^2 - a^2) - m(a^2 + b^2)) + \frac{ab}{2} (\lambda(a+b) + m(a-b))$
 $= \frac{m}{12} (2b^3 - 2a^3 - 3(b-a)(a^2 + b^2) + 6ab(a-b)) - \frac{\lambda}{12} (2b^3 + 2a^3 + 3(b-a)(b^2 - a^2) - 6ab(a+b))$
 $= \frac{m}{12} (a^3 - b^3 + 3a^2b - 3ab^2) + \frac{\lambda}{12} (b^3 + a^3 + 3a^2b + 3ab^2)$

Flux vanishes when $\lambda = \frac{m(b-a)(a^2 + 4ab + b^2)}{(a+b)^3}$

In the special case $a=b$, $\lambda=0$, $D=B=0 \Rightarrow w(0)=0$
 i.e. asymmetric velocity profile



2.



$$h = h_0 + \Delta h x / L$$

(a) For lubrication regime : $h_0/L \ll 1$ (thin gap)

and $\left| \rho u \frac{\partial u}{\partial x} \right| \ll \left| \mu \frac{\partial^2 u}{\partial z^2} \right|$ (negligible inertia)

$$\Rightarrow \frac{\rho u h^2}{L \mu} \ll 1$$

but from mass conservation $\frac{u}{L} \sim \frac{V}{h} \Rightarrow \frac{\rho V h}{\mu} \ll 1$

(b) Lubrication equation $0 = -\frac{\partial p}{\partial x}$ and $0 = -\frac{\partial p}{\partial x} + \mu \frac{\partial^2 u}{\partial z^2}$

Subject to $u(0) = u(h) = 0 \Rightarrow u = \frac{\partial p}{\partial x} \frac{1}{2\mu} (z^2 - hz)$

Fluid flux per unit width $q = \int_0^h u dz = -\frac{h^3}{12\mu} \frac{\partial p}{\partial x}$

(c) Mass conservation (pointwise) $\frac{du}{dx} + \frac{dw}{dz} = 0$

$$\Rightarrow \int_0^h \frac{du}{dx} dz + [w]_0^h = 0$$

$$\Rightarrow \frac{\partial}{\partial x} \int_0^h u dz - u(h) \frac{\partial h}{\partial x} + w(h) = 0$$

$$\Rightarrow \frac{\partial q}{\partial x} = V \quad \text{since } w(h) = -V$$

Integrating $q(L) - q(-L) = 2VL$ — (1)

(d) $\frac{\partial p}{\partial x} = -\frac{12\mu q}{h^3}$. Then integrate $\int_{-L}^L \frac{dp}{dx} dx = \int_{-L}^L \frac{-12\mu q}{h^3} dx$

but no imposed pressure gradient $\Rightarrow p(L) = p(-L) \Rightarrow \int_{-L}^L \frac{q}{h^3} dx = 0$

Integrate by parts $\left[\frac{L}{-2\Delta h} q \left(h_0 + \frac{\Delta h x}{L} \right)^{-2} \right]_{-L}^L + \int_{-L}^L \frac{L}{2\Delta h} \left(h_0 + \frac{\Delta h x}{L} \right)^{-2} \frac{dq}{dx} dx = 0$

$$\Rightarrow \frac{-L}{2\Delta h} \left(\frac{q(L)}{(h_0 + \Delta h)^2} - \frac{q(-L)}{(h_0 - \Delta h)^2} \right) + \frac{LV}{2\Delta h} \left[-\frac{L}{\Delta h} \left(h_0 + \frac{\Delta h x}{L} \right)^{-1} \right]_{-L}^L = 0$$

$$\Rightarrow - \left(\frac{q(L)}{(h_0 + \Delta h)^2} - \frac{q(-L)}{(h_0 - \Delta h)^2} \right) + \frac{-VL}{\Delta h} \left(\frac{1}{h_0 + \Delta h} - \frac{1}{h_0 - \Delta h} \right) = 0$$

$$\Rightarrow \frac{q(L)}{(h_0 + \Delta h)^2} - \frac{q(-L)}{(h_0 - \Delta h)^2} = \frac{2VL\Delta h}{\Delta h (h_0 + \Delta h)(h_0 - \Delta h)}$$

$$\Rightarrow q(L)(h_0 - \Delta h)^2 - q(-L)(h_0 + \Delta h)^2 = 2VL(h_0 + \Delta h)(h_0 - \Delta h) \quad \text{--- (2)}$$

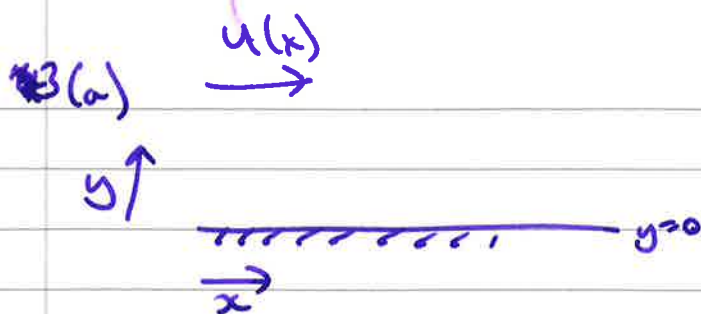
Solve --- (1) and --- (2)

$$\Rightarrow q(L) [(h_0 - \Delta h)^2 - (h_0 + \Delta h)^2] + 2VL(h_0 + \Delta h)^2 = 2VL(h_0^2 - \Delta h^2)$$

$$\Rightarrow q(L) \cdot -4h_0\Delta h = 2VL(h_0^2 - \cancel{\Delta h^2} - \cancel{h_0^2} - 2\Delta h h_0 - \cancel{\Delta h^2}) = -4VL(h_0\Delta h + \Delta h^2)$$

$$\Rightarrow q(L) = \frac{VL}{h_0} (h_0 + \Delta h) = VL \left(1 + \frac{\Delta h}{h_0} \right)$$

10 and $q(-L) = -VL \left(1 - \frac{\Delta h}{h_0} \right)$



- $u(x)$ does not satisfy no-slip condition on $y=0$
 $\Rightarrow$ boundary layer within which viscous processes reduce u .
- $\underline{u} = (u, v)$

Boundary layer equations
(Steady)

$$\begin{aligned} \frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} &= 0 \\ u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y} &= -\frac{1}{\rho} \frac{\partial p}{\partial x} + \nu \frac{\partial^2 u}{\partial y^2} \\ 0 &= -\frac{1}{\rho} \frac{\partial p}{\partial y} \end{aligned}$$

Justified as follows • $\left| \frac{\partial^2 u}{\partial y^2} \right| \gg \left| \frac{\partial^2 u}{\partial x^2} \right|$ since $1 \gg (\delta/L)^2$

- $\left| -\frac{1}{\rho} \frac{\partial p}{\partial y} \right| \gg \left| u \frac{\partial v}{\partial x} \right|$ since $\frac{p}{\rho L} \gg \frac{u v}{L} = \frac{u^2 \delta}{L^2}$

OK since $p \propto u^2 \Rightarrow 1 \gg \delta^2/L^2$

- $\left| -\frac{1}{\rho} \frac{\partial p}{\partial y} \right| \gg \left| v \frac{\partial^2 v}{\partial y^2} \right|$ since $\frac{p}{\rho L} \gg \frac{v^2}{L^2} = \frac{v u}{L}$

OK since $1 \gg \frac{1}{Re}$ $Re = \frac{u L}{\nu}$

Results in lectures + derivation

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Similar Method
to examples

(b) Balance viscous and inertial terms to estimate boundary layer thickness

$$\nu \frac{u}{\delta^2} \sim \frac{u^2}{x} \Rightarrow \delta^2 \sim \frac{\nu x}{u} = \frac{\nu x^2}{U} \Rightarrow \delta \sim \left(\frac{\nu x}{U} \right)^{1/2}$$

(c) Introduce streamfunction $u = \frac{\partial \psi}{\partial y}$ $v = -\frac{\partial \psi}{\partial x}$ Define $\delta = \left(\frac{\nu x}{U} \right)^{1/2}$

and $\psi = -\frac{U}{x} \cdot \delta(x) \cdot f\left(\frac{y}{\delta(x)}\right) = -\left(\frac{\nu x}{U}\right)^{1/2} f\left(\frac{y}{\delta}\right)$ $\left[\xi = y/\delta \right]$

$$u = \frac{\partial \psi}{\partial y} = -\left(\frac{\nu x}{U}\right)^{1/2} f' \quad v = -\frac{\partial \psi}{\partial x} = \left(\frac{\nu x}{U}\right)^{1/2} \xi f' = \frac{\nu}{U} \xi f'$$

$$\frac{\partial u}{\partial x} = +\frac{(2\Gamma)^{1/2}}{\delta^2} \delta' f' + \frac{(2\Gamma)^{1/2}}{\delta} \cdot \frac{\delta'}{\delta} f'' = \frac{(2\Gamma)^{1/2}}{\delta} \left[+\frac{f'}{x} + \frac{\delta f''}{x} \right]$$

$$\frac{\partial u}{\partial y} = -\frac{(2\Gamma)^{1/2}}{\delta^2} f'' \quad , \quad \frac{\partial^2 u}{\partial y^2} = -\frac{(2\Gamma)^{1/2}}{\delta^3} f'''$$

Pressure gradient $-\frac{1}{\rho} \frac{\partial p}{\partial x} = 4 \cdot u' = -\frac{\Gamma}{x} + \frac{\Gamma}{x^2}$

$$-\frac{(2\Gamma)^{1/2}}{\delta} f' \cdot \frac{(2\Gamma)^{1/2}}{\delta} \left[+\frac{f'}{x} + \frac{\delta f''}{x} \right] + \frac{(2\Gamma)^{1/2}}{x} \delta f' \cdot \frac{(2\Gamma)^{1/2}}{\delta^2} f'' = -\frac{\Gamma^2}{x^3} + \frac{2(2\Gamma)^{1/2}}{\delta^3} f'''$$

$$\Rightarrow \frac{2\Gamma}{x^2} \cdot \frac{f'^2}{x} = -\frac{\Gamma^2}{x^3} + \frac{2(2\Gamma)^{1/2}}{(2\Gamma)^{1/2} x^3} f'''$$

$$\Rightarrow f'^2 = 1 + f''' \quad \text{--- (1)}$$

Boundary conditions (i) $u(0) = 0 \Rightarrow f'(0) = 0$

(ii) $v(0) = 0$ (automatically satisfied)

(iii) $u \rightarrow -\frac{\Gamma}{x} \Rightarrow f' \rightarrow 1$ as $\delta \rightarrow \infty$

(a) If $u = -\frac{\Gamma}{x} (3 \tanh^2(A + B\delta) - 2)$ then $f' = 3 \tanh^2(A + B\delta) - 2$

So $f'' = 6B \tanh(\dots) \operatorname{sech}^2(\dots) = 6B [\tanh(\dots) - \tanh^3(\dots)]$

$$f''' = 6B^2 \operatorname{sech}^2(\dots) - 18B^2 \tanh^2(\dots) \operatorname{sech}^2(\dots)$$

$$= 6B^2 (1 - \tanh^2(\dots)) - 18B^2 \tanh^2(\dots) (1 - \tanh^2(\dots))$$

Substitute into (1): $18B^2 \tanh^4(\dots) - 24B^2 \tanh^2(\dots) + 6B^2$
 $- (3 \tanh^2(\dots) - 2)^2 + 1 = 0$

$$\Rightarrow (18B^2 - 9) \tanh^4(\dots) + (12 - 24B^2) \tanh^2(\dots) + 6B^2 - 4 + 1 = 0$$

$$\Rightarrow B^2 = \frac{1}{2} \Rightarrow B = \frac{1}{\sqrt{2}}$$

Checking boundary conditions $f' \rightarrow 1$ as $\delta \rightarrow \infty$ ✓

$$f'(0) = 0 \Rightarrow 3 \tanh^2 A = 2$$

$$\Rightarrow A = \tanh^{-1} \left(\frac{2}{3} \right)^{1/2}$$

unseen example

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Unseen example, but straightforward method close to Reynolds in plates

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4(a) Vorticity $\underline{\omega} = \nabla \wedge \underline{u}$

$$\begin{aligned} [\underline{u} \wedge \underline{\omega}]_i &= \epsilon_{ijk} u_j \epsilon_{klm} \omega_m = (\delta_{il} \delta_{jm} - \delta_{im} \delta_{jl}) u_j \omega_m \\ &= u_j \omega_j - u_j \omega_j \\ &= \nabla_i (|\underline{u}|^2 / 2) - \underline{u} \cdot \nabla \underline{u}_i \end{aligned}$$

Euler equation $\frac{d\underline{u}}{dt} + \underline{u} \cdot \nabla \underline{u} = -\frac{1}{\rho} \nabla p$

$$\Rightarrow \frac{d\underline{u}}{dt} = \underline{u} \wedge \underline{\omega} - \nabla \left(\frac{p}{\rho} + \frac{1}{2} |\underline{u}|^2 \right)$$

$$\Rightarrow \frac{d\underline{\omega}}{dt} = \nabla \wedge (\underline{u} \wedge \underline{\omega})$$

$$\begin{aligned} [\nabla \wedge (\underline{u} \wedge \underline{\omega})]_i &= \epsilon_{ijk} \nabla_j \epsilon_{klm} u_m \omega_l = (\delta_{il} \delta_{jm} - \delta_{im} \delta_{jl}) \nabla_j u_m \omega_l \\ &= \nabla_j u_i \omega_j - \nabla_j u_j \omega_i \\ &= (\underline{\omega} \cdot \nabla \underline{u})_i - [(\underline{u} \cdot \nabla) \underline{\omega}]_i \end{aligned}$$

Hence Vorticity equation $\frac{d\underline{\omega}}{dt} + \underline{u} \cdot \nabla \underline{\omega} = \underline{\omega} \cdot \nabla \underline{u}$

For 2-D flow $\underline{\omega} \cdot \nabla \underline{u} \equiv 0 \Rightarrow \frac{d\underline{\omega}}{dt} + \underline{u} \cdot \nabla \underline{u} = 0$

(b) Vorticity $\underline{\omega} = \nabla \wedge V(r) \hat{z} = \left(\frac{\partial V}{\partial r} + \frac{V}{r} \right) \hat{z} = \frac{1}{r} \frac{\partial}{\partial r} (rV) \hat{z} \equiv R \hat{z}$

(c) $\underline{u}_1 = \frac{1}{r} \frac{\partial \psi}{\partial \theta} \hat{r} - \frac{\partial \psi}{\partial r} \hat{\theta}$ Vorticity $\nabla \wedge \underline{u}_1 = -\left(\frac{1}{r} \frac{\partial}{\partial r} (r \frac{\partial \psi}{\partial r}) + \frac{1}{r^2} \frac{\partial^2 \psi}{\partial \theta^2} \right) \hat{z}$

Vorticity $= (R - \nabla^2 \psi) \hat{z}$ $|R| \gg |\nabla^2 \psi|$ (small perturbation)

$$\frac{\partial}{\partial t} (R - \nabla^2 \psi) + \left(V(r) \hat{\theta} + \frac{1}{r} \frac{\partial \psi}{\partial \theta} \hat{r} - \frac{\partial \psi}{\partial r} \hat{\theta} \right) \cdot \nabla (R - \nabla^2 \psi) = 0$$

linearise to $\frac{\partial}{\partial t} (-\nabla^2 \psi) - V(r) \hat{\theta} \cdot \nabla (\nabla^2 \psi) + \left(\frac{1}{r} \frac{\partial \psi}{\partial \theta} \hat{r} - \frac{\partial \psi}{\partial r} \hat{\theta} \right) \cdot \nabla R = 0$

$$\Rightarrow \left(\frac{\partial}{\partial t} + \frac{V}{r} \frac{\partial}{\partial \theta} \right) \left(\frac{1}{r} \frac{\partial}{\partial r} (r \frac{\partial \psi}{\partial r}) + \frac{1}{r^2} \frac{\partial^2 \psi}{\partial \theta^2} \right) - \frac{dR}{dr} \frac{1}{r} \frac{\partial \psi}{\partial \theta} = 0$$

Result given in lectures

Easy

but cartesian
under example in lectures

(d) write $\psi = \phi(r) \exp(st + i n \theta)$

$$(s + i n \frac{V}{r}) \left(\frac{1}{r} \frac{d}{dr} (r \frac{d\phi}{dr}) - \frac{n^2}{r^2} \phi \right) = \frac{1}{r} \frac{d^2}{dr^2} \phi$$

$$\Rightarrow \frac{1}{r} \frac{d}{dr} (r \frac{d\phi}{dr}) - \frac{n^2}{r^2} \phi = \frac{i n}{s + i n V/r} \frac{1}{r} \frac{d^2}{dr^2} \phi$$

Multiply by ϕ^*

$$\int_{R_1}^{R_2} \phi^* \frac{d}{dr} (r \frac{d\phi}{dr}) dr - n^2 \int_{R_1}^{R_2} \frac{|\phi|^2}{r} dr = \int_{R_1}^{R_2} \frac{i n}{s + i n V/r} \frac{d^2}{dr^2} |\phi|^2 dr \quad (*)$$

Use integration by parts

$$\int_{R_1}^{R_2} \phi^* \frac{d}{dr} (r \frac{d\phi}{dr}) dr = \left[\phi^* r \frac{d\phi}{dr} \right]_{R_1}^{R_2} - \int_{R_1}^{R_2} r \left| \frac{d\phi}{dr} \right|^2 dr$$

since $\phi(R_1) = \phi(R_2) = 0$

Write $s = s_r + i s_i$

$$\frac{i n (s_r - i s_i - i n V/r)}{s_r^2 + (s_i + n V/r)^2} = \frac{i n}{s + i n V/r}$$

$$\text{Take Im} \{ (*) \} \Rightarrow s_r \int_{R_1}^{R_2} \frac{1}{s_r^2 + (s_i + n V/r)^2} \frac{d^2}{dr^2} |\phi|^2 dr = 0$$

For instability, require $s_r > 0$

$$\Rightarrow \frac{d^2}{dr^2} = 0 \text{ at some point in } R_1 < r < R_2$$

unseen, but quite similar to Cartesian result

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