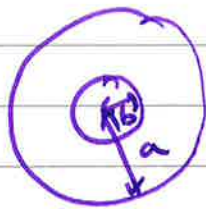


Advanced Fluids 2017



$$u = w(r) \hat{e}_\theta \quad a \leq r \leq b$$

(a) $\frac{1}{r} \frac{d}{dr} (r \frac{dw}{dr}) = 0$ subject to $w(a) = V_2$ $w(b) = V_1$

$$w = A \log r + B$$

$$A \log a + B = V_2$$

$$A \log b + B = V_1$$

$$\Rightarrow A \log \frac{a}{b} = V_2 - V_1 \quad \text{and} \quad B = V_2 - \frac{(V_2 - V_1) \log a}{\log a/b}$$

$$\text{Here } w = \frac{(V_2 - V_1)}{\log a/b} \log r + V_2 - \frac{(V_2 - V_1) \log a}{\log a/b}$$

$$= V_2 + (V_2 - V_1) \frac{\log r/a}{\log a/b}$$

(b) Viscous dissipation per unit axial length $= 2\pi \int_0^{2\pi} \int_a^b e_{ij} e_{ij} r dr d\theta$

$$e_{ij} = \frac{1}{2} \begin{pmatrix} 0 & 0 & 2r \frac{\partial w}{\partial r} \\ 2r \frac{\partial w}{\partial r} & 0 & 0 \\ 0 & 0 & 0 \end{pmatrix} \quad e_{ij} e_{ij} = \frac{1}{2} \left(\frac{\partial w}{\partial r} \right)^2 = \frac{1}{2} \left[\frac{(V_2 - V_1)}{\log a/b} \frac{1}{r} \right]^2$$

$$\text{Viscous dissipation} = 4\pi \mu \frac{1}{2} \int_a^b \left(\frac{V_2 - V_1}{\log a/b} \right)^2 \frac{1}{r} dr$$

$$= 2\pi \mu \frac{(V_2 - V_1)^2}{\log a/b}$$

(c) Net Flux $Q = 2\pi \int_b^a r w dr = 2\pi \left[\frac{V_2 r^2}{2} + \frac{(V_2 - V_1)}{\log a/b} \left(\frac{r^2}{2} \log \frac{r}{a} - \frac{1}{4} r^2 \right) \right]_b^a$

$$= \pi (V_2 (a^2 - b^2) + \frac{V_2 - V_1}{\log a/b} (-\frac{1}{2} a^2 - b^2 \log \frac{b}{a} + \frac{1}{2} b^2))$$

For $Q=0$ $0 = V_2 (a^2 - b^2) + \frac{(V_2 - V_1)}{\log a/b} \left(\frac{1}{2} b^2 - \frac{1}{2} a^2 - b^2 \log \frac{b}{a} \right)$

define $R = \frac{a}{b}$ $0 = V_2 (R^2 - 1) + \frac{(V_2 - V_1)}{\log R} \left(\frac{1}{2} - \frac{1}{2} R^2 + \log R \right)$

1. unseen, although flow driven by pressure gradient in lecture

6. unseen, similar to lecture example

unseen

$$0 = V_2 (R^2 \log R - \log R + \frac{1}{2} - \frac{1}{2} R^2 + \log R) \\ - V_1 (\frac{1}{2} - \frac{1}{2} R^2 + \log R)$$

$$\Rightarrow V_2 = V_1 \left[\frac{\log R^2 + 1 - R^2}{R^2 \log R^2 + 1 - R^2} \right]$$

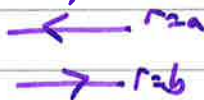
5

When $R = 1 + \epsilon$ ($\epsilon \ll 1$) $R^2 = 1 + 2\epsilon + \epsilon^2$
 $\log R^2 = 2 \log R = 2(\epsilon - \epsilon^2/2 + \dots)$

$$V_2 = V_1 \left[\frac{2\epsilon - \epsilon^2 + 1 - 1 - 2\epsilon - \epsilon^2 + \dots}{(1 + 2\epsilon + \epsilon^2)(2\epsilon - \epsilon^2) + 1 - 1 - 2\epsilon - \epsilon^2} \right] \\ = V_1 \left[\frac{-2\epsilon^2 + \dots}{2\epsilon - \epsilon^2 + 4\epsilon^2 - 2\epsilon - \epsilon^2 + \dots} \right] = -V_1 + \dots$$

2

Alternatively argue that when $R = 1 + \epsilon$, symmetry demands $V_2 = -V_1$,



(a) Now solve $\mu \frac{1}{r} \frac{d}{dr} (r \frac{dw}{dr}) = -G$

$$\Rightarrow w = A \log r + B - \frac{Gr^2}{4} \quad w(a) = 0 \quad w(b) = V_1 \\ \text{or } \frac{dw}{dr} = \frac{A}{r} - \frac{Gr}{2}$$

From boundary conditions $A \log a + B - \frac{Ga^2}{4} = 0$? $A \log \frac{a}{b} = \frac{G}{4} (a^2 - b^2)$
 or $A \log b + B - \frac{Gb^2}{4} = V_1$ $\frac{G}{4} (a^2 - b^2) = V_1$

Viscous dissipation $\dot{\epsilon}$ per unit length $= 2\pi\mu \int_b^a \left(\frac{A}{r} - \frac{Gr}{2} \right)^2 r dr = 2\pi\mu \int_b^a \frac{A^2}{r} - \frac{GA}{r} + \frac{1}{4} \frac{G^2 r^3}{\mu^2} dr$
 $= 2\pi\mu \left(A^2 \log \frac{a}{b} - \frac{GA}{2} (a^2 - b^2) + \frac{1}{16} \frac{G^2}{\mu^2} (a^4 - b^4) \right)$

Minimise wrt V_1 : $\frac{\partial \dot{\epsilon}}{\partial V_1} = \frac{\partial \dot{\epsilon}}{\partial A} \frac{\partial A}{\partial V_1} = 0$
 $\Rightarrow \left[2A \log \frac{a}{b} - \frac{G}{2} (a^2 - b^2) \right] \frac{\partial A}{\partial V_1} = 0$

$\Rightarrow V_1 = 0$ to minimise viscous dissipation.

Alternatively : argue that must minimise work done by boundary $\Rightarrow V_1 = 0$

under

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2.(a) Derive $u_r = \frac{1}{r} \frac{\partial \psi}{\partial \theta}$ $u_\theta = -\frac{\partial \psi}{\partial r}$

Vorticity $\omega = \frac{1}{r} \frac{\partial}{\partial r}(r u_\theta) - \frac{1}{r} \frac{\partial u_r}{\partial \theta} = -\frac{1}{r} \frac{\partial}{\partial r}(r \frac{\partial \psi}{\partial r}) - \frac{1}{r} \frac{\partial^2 \psi}{\partial \theta^2} = -\nabla^2 \psi$

Also vorticity is $\perp$ to plane at flow is 2-D $\Rightarrow \underline{\omega} = \omega \hat{z}$.

(b) Stokes flow $0 = -\nabla p + \mu \nabla^2 \underline{u}$

Curl $0 = \mu \nabla^2 \nabla \times \underline{u} \Rightarrow \nabla^4 \psi = 0$

(c) In far-field $\psi = \psi_\infty = E x y$ in Cartesian coordinates
 $= E r^2 \cos \theta \sin \theta$
 $= \frac{1}{2} E r^2 \sin 2\theta$ in polar

(d) Since $\psi \propto \sin 2\theta$ in far-field, seek a complete solution with $\psi = f(r) \sin 2\theta$.

$$\nabla^2 \psi = \left(\frac{1}{r} (r f')' - 4f \right) \sin 2\theta$$

And if $f(r) = r^\alpha$ $\nabla^2 \psi = (\alpha^2 - 4) r^{\alpha-2} \sin 2\theta$.

Then $\nabla^4 \psi = (\alpha^2 - 4)(\alpha - 2)(\alpha - 4) r^{\alpha-4} \sin 2\theta$.

Possible solutions $\alpha = \pm 2, 4, 0$.

Seek solution of form $\psi = (A r^2 + B + C r^{-2} + D r^4) \sin 2\theta$.

Boundary conditions: (i) $\psi \rightarrow \psi_\infty$ as $r \rightarrow \infty$ (far-field)

(ii) $u_r = 0$ } or $r = a$ (no slip)

(iii) $u_\theta = 0$ }

From (i): $D = 0$ and $A = E/2$

From (ii) $\frac{\partial \psi}{\partial r} = 0 \Rightarrow A a^2 + B + \frac{C}{a^2} = 0$

From (iii) $\frac{\partial \psi}{\partial r} = 0 \Rightarrow 2Aa - 2C/a^3 = 0$

Here $C = \frac{E}{2}a^4$. $B = -\frac{E}{2}a^2 - \frac{E}{2}a^2 = -Ea^2$

$$\psi = \left(\frac{E}{2}r^2 - Ea^2 + \frac{E}{2}\frac{a^4}{r^2} \right) \sin 2\theta$$

$$= \frac{E}{2} \left(r - \frac{a^2}{r} \right)^2 \sin 2\theta.$$

(c) Flow field $u_r = \frac{1}{r} \frac{\partial \psi}{\partial \theta} = \frac{1}{r} E \left(r - \frac{a^2}{r} \right)^2 \cos 2\theta$.

$$u_\theta = -\frac{\partial \psi}{\partial r} = E \left(r - \frac{a^2}{r} \right) \left(1 + \frac{a^2}{r^2} \right) \sin 2\theta.$$

On surface of disk $\underline{n} = -\underline{\hat{r}}$ (normal vector)

Need to evaluate $\underline{t} \cdot \underline{\sigma} \cdot \underline{n}$ where $\underline{t}$ is tangential vector ($\underline{t} = \underline{\hat{\theta}}$)

i.e. $\underline{t} \cdot \underline{\sigma} \cdot \underline{n} = -\sigma_{r\theta}$.

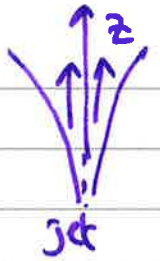
$$\sigma_{r\theta} = 2\mu e_{r\theta} = \mu \left(r \frac{\partial}{\partial r} \left(\frac{u_\theta}{r} \right) + \frac{1}{r} \frac{\partial u_r}{\partial \theta} \right) \Big|_{r=a}$$

$$= \mu r \frac{\partial}{\partial r} \left(E \left(1 - \frac{a^4}{r^4} \right) \sin 2\theta \right) + \frac{1}{r} E \frac{\partial}{\partial \theta} \left(r - \frac{a^2}{r} \right)^2 \sin 2\theta \Big|_{r=a}$$

$$= 4\mu E \sin 2\theta$$

So tangential stress exerted by fluid on disk = $4\mu E \sin 2\theta$.

3(a) Navier Stokes



$$\rho \left(\frac{\partial w}{\partial t} + u \frac{\partial w}{\partial r} + w \frac{\partial w}{\partial z} \right) = -\frac{\partial p}{\partial z} + \mu \left(\frac{1}{r} \frac{\partial}{\partial r} \left(r \frac{\partial w}{\partial r} \right) + \frac{\partial^2 w}{\partial z^2} \right)$$

$$\frac{1}{r} \frac{\partial}{\partial r} (r u) + \frac{\partial w}{\partial z} = 0$$

Thin jet $\Rightarrow r/z \ll 1$ (r & z typical lengths)

$\Rightarrow u \sim \frac{r}{z} w$ (radial velocity is small)

Steady $\Rightarrow \frac{\partial w}{\partial t} = 0$

Thin $\Rightarrow \frac{1}{r} \frac{\partial}{\partial r} \left(r \frac{\partial w}{\partial r} \right) \gg \frac{\partial^2 w}{\partial z^2}$

^{imposed}
No pressure gradient $\Rightarrow \frac{\partial p}{\partial z} = 0$

Remaining radial terms of axial momentum equation $u \frac{\partial w}{\partial r} \sim w \frac{\partial w}{\partial z}$

And these must balance viscous stresses at leading order

4 $\Rightarrow u \frac{\partial w}{\partial r} + w \frac{\partial w}{\partial z} = \frac{\nu}{r} \frac{\partial}{\partial r} \left(r \frac{\partial w}{\partial r} \right)$

(b) $F = 2\pi\rho \int_0^\infty r w^2 dr$

$$\frac{dF}{dz} = 2\pi\rho \int_0^\infty 2r w \frac{\partial w}{\partial z} dr = 2\pi\rho \int_0^\infty 2r \left(\frac{\nu}{r} \frac{\partial}{\partial r} \left(r \frac{\partial w}{\partial r} \right) - u \frac{\partial w}{\partial r} \right) dr$$

$$= \left[4\pi\rho \nu r \frac{\partial w}{\partial r} \right]_0^\infty - 4\pi\rho \int_0^\infty \frac{\partial}{\partial r} (r u w) - w \frac{\partial}{\partial r} (r u) dr$$

$$= \left[4\pi\rho \left(\nu r \frac{\partial w}{\partial r} - r u w \right) \right]_0^\infty + 4\pi\rho \int_0^\infty r w \frac{\partial w}{\partial z} dr$$

$$= \left[4\pi\rho \left(\nu r \frac{\partial w}{\partial r} - r u w \right) \right]_0^\infty - \frac{dF}{dz}$$

2-D (Cartesian) example in lectures

Similar to 2-D manipulation

In the far-field $w \rightarrow 0$ as $r \rightarrow \infty$
 $\frac{\partial w}{\partial r} \rightarrow 0$

Here $\frac{dF}{dz} = 0$

$\Rightarrow F = 2\pi\rho \int_0^{\infty} r w^2 dr = \text{constant}$

(c) Scaling analysis $F \sim \rho \delta^2 w^2$ $w \sim v z / \delta^2$
 and $\frac{w^2}{z} \sim \frac{v w}{\delta^2}$ $F \sim \rho \delta^2 \cdot \frac{v^2 z^2}{\delta^4}$

$\Rightarrow \delta^2 \sim \frac{v^2 \rho z^2}{F} \Rightarrow \delta \sim v z \left(\frac{\rho}{F}\right)^{1/2}$

and $w \sim v z \frac{F}{v^2 \rho z^2} \Rightarrow w \sim \frac{F}{\rho v z}$

(d) Define $\delta(z) = v z \left(\frac{\rho}{F}\right)^{1/2}$ $\eta = r/\delta(z)$

Stokes stream function $\Psi = v z^2 \frac{\rho}{F} \cdot \frac{F}{\rho} \frac{1}{v z} f(\eta) = v z f(\eta)$

$u = -\frac{1}{r} \frac{\partial \Psi}{\partial z} = -\frac{1}{r} (v f + v z \frac{\partial \eta}{\partial z} f')$ $\frac{\partial \eta}{\partial z} = \frac{r}{\delta^2} \delta' = -\frac{\eta}{2}$
 $= -\frac{1}{r} v (f - \frac{\eta}{2} f')$ $\frac{\partial \eta}{\partial r} = \frac{1}{\delta}$

$w = \frac{1}{r} \frac{\partial \Psi}{\partial r} = \frac{v z}{r} \cdot \frac{1}{\delta} f' = \left(\frac{F}{\rho}\right)^{1/2} \frac{1}{r} f'$

$\frac{\partial w}{\partial r} = \left(\frac{F}{\rho}\right)^{1/2} \left(-\frac{1}{r^2} f' + \frac{1}{r} \frac{1}{\delta} f''\right)$

$\frac{1}{r} \frac{\partial}{\partial r} (r \frac{\partial w}{\partial r}) = \frac{1}{r} \frac{\partial}{\partial r} \left(\frac{F}{\rho}\right)^{1/2} \left(-\frac{1}{r^2} f' + \frac{1}{r} \frac{1}{\delta} f''\right) = \frac{1}{r} \left(\frac{F}{\rho}\right)^{1/2} \left(\frac{1}{r^2} f' - \frac{1}{r} \frac{1}{\delta} f'' + \frac{1}{\delta^2} f'''\right)$

$\frac{\partial w}{\partial z} = \left(\frac{F}{\rho}\right)^{1/2} \frac{1}{r} \cdot \frac{\eta}{2} f''$

Governing equation: $-\frac{v}{r} (f - \frac{\eta}{2} f') \left(\frac{F}{\rho}\right)^{1/2} \left(\frac{1}{r^2} f' + \frac{1}{\delta} f''\right)$
 $+ \left(\frac{F}{\rho}\right)^{1/2} \frac{1}{r} f' \cdot \left(\frac{F}{\rho}\right)^{1/2} \frac{1}{r} \cdot \frac{\eta}{2} f'' = \frac{v}{r} \left(\frac{F}{\rho}\right)^{1/2} \left(\frac{1}{r^2} f' - \frac{1}{r} \frac{1}{\delta} f'' + \frac{1}{\delta^2} f'''\right)$

Standard methods, but under

Given example, but follows many examples

$$-\frac{\nu}{r^3}(f-yf')(-f'+yf'') + \left(\frac{F}{\rho}\right)^{\frac{1}{2}} \frac{-y}{r^{\frac{3}{2}}} f'f''$$

$$= \frac{\nu}{r^3}(f' - yf'' + y^2f''')$$

$$\Rightarrow (f-yf')(f'-yf'') + \left(\frac{F}{\rho}\right)^{\frac{1}{2}} \frac{-y}{r^{\frac{3}{2}}} f'f''$$

$$= f' - yf'' + y^2f'''$$

$$\text{but } \left(\frac{F}{\rho}\right)^{\frac{1}{2}} \frac{r}{r^{\frac{3}{2}}} = \frac{r}{\delta} = y$$

$$\Rightarrow (f-yf')(f'-yf'') - y^2f'f'' = f' - yf'' + y^2f'''$$

$$\Rightarrow ff' - y(f'^2 + ff'') = f' - yf'' + y^2f'''$$

(e) Boundary conditions:

$$(i) \text{ ~~w(\delta) = 0~~ } w \rightarrow 0 \text{ as } r \rightarrow \infty \Rightarrow f' \rightarrow 0 \text{ as } y \rightarrow \infty$$

$$(ii) u(0) = 0 \Rightarrow f(0) = 0$$

$$(iii) 2\pi \int_0^\infty \rho r w^2 dr = F \Rightarrow 2\pi \int_0^\infty \rho \cdot \delta \cdot y \cdot \frac{F}{\rho} \frac{1}{\delta^{\frac{3}{2}}} f'^2 \cdot \delta dy = F$$

$$\Rightarrow 2\pi \int_0^\infty \frac{f'^2}{y} dy = 1$$

Similar to
Example 9.2.1

4(a) Vortex sheet $u_0 = \begin{cases} u_0 \hat{x} & z > 0 \\ -u_0 \hat{x} & z < 0 \end{cases}$ $p_0 = \text{constant}$

Perturbation equations $\nabla \cdot \underline{u}_1 = 0$

$$\rho \left(\frac{d\underline{u}_1}{dt} + \underline{u}_0 \cdot \nabla \underline{u}_1 + \underline{u}_1 \cdot \nabla \underline{u}_0 \right) = -\nabla p_1$$

$$\Rightarrow \text{as } \underline{u}_0 \text{ piecewise constant } \rho \left(\frac{d}{dt} + \underline{u}_0 \cdot \nabla \right) \underline{u}_1 = -\nabla p_1$$

Take divergence $\Rightarrow \nabla^2 p_1 = 0$

Take ∇^2 of Euler equation $\Rightarrow \nabla^2 \underline{u}_1 = 0$

If $\underline{u}_1$ and p_1 proportional to $e^{i(kx+ly)+st}$

write $\underline{u}_1 = \begin{pmatrix} u_1(z) \\ v_1(z) \\ w_1(z) \end{pmatrix} e^{i(kx+ly)+st}$ and $p_1 = \hat{p}_1(z) e^{i(kx+ly)+st}$

Since $\nabla^2 \underline{u}_1 = 0 \Rightarrow \frac{d^2}{dz^2} \begin{pmatrix} u_1 \\ v_1 \\ w_1 \end{pmatrix} - (k^2 + l^2) \begin{pmatrix} u_1 \\ v_1 \\ w_1 \end{pmatrix} = 0$ and similarly for $\hat{p}_1(z)$

Pick solution that decays away from interface

$$u_1 = \begin{cases} A e^{-\Delta z} & z > 0 \\ B e^{\Delta z} & z < 0 \end{cases} \quad \Delta^2 = k^2 + l^2$$

$$\text{or } v_1 = \begin{cases} C e^{-\Delta z} & z > 0 \\ D e^{\Delta z} & z < 0 \end{cases} \quad w_1 = \begin{cases} E e^{-\Delta z} & z > 0 \\ F e^{\Delta z} & z < 0 \end{cases}$$

Boundary conditions:

(i) Kinematic condition linearizes to $\left(\frac{d}{dt} + \underline{u}_0 \cdot \nabla \right) y = w$

$$\Rightarrow \begin{aligned} (s + i u_0 k) y_0 &= E \\ (s - i u_0 k) y_0 &= F \end{aligned}$$

2D perturbations in lectures + Squire's Th. The axis for 3D perturbation

(ii) Dynamic condition: p is continuous $\Rightarrow p_1(0^+) = p_1(0^-)$
 $\Rightarrow \partial_x p_1(x=0^+) = \partial_x p_1(x=0^-)$

$$\Rightarrow (s + ikU_0)A = (s - ikU_0)B \quad \text{from Euler equation}$$

Likewise $(s + ikU_0)C = (s - ikU_0)D$

Incompressibility $\Rightarrow ikA + iC - \Delta E = 0$
 and $ikB + iD + \Delta F = 0$

Hence $(s + ikU_0)\Delta E = (s - ikU_0)\Delta F$

$$\Rightarrow (s + ikU_0)^2 = -(s - ikU_0)^2$$

$$\Rightarrow s^2 + 2ikU_0s - k^2U_0^2 = -s^2 + 2ikU_0s + k^2U_0^2$$

$$\Rightarrow s^2 = k^2U_0^2$$

$\Rightarrow s = \pm kU_0$ Growth rate

(b) $\underline{u} = (u(x), +E_y, -E_z)$

$$\underline{\omega} = \nabla \wedge \underline{u} = \begin{vmatrix} \frac{\partial}{\partial x} & \frac{\partial}{\partial y} & \frac{\partial}{\partial z} \\ u & +E_y & -E_z \end{vmatrix} = \frac{\partial u}{\partial z} \hat{y} \quad \text{Hence } \omega = \frac{\partial u}{\partial z}$$

Vorticity equation $\frac{\partial \omega}{\partial t} + \underline{u} \cdot \nabla \omega = \omega \cdot \nabla u + \nu \nabla^2 \omega$

Hence $-Ez \frac{\partial \omega}{\partial t} = +\omega E + \nu \frac{\partial^2 \omega}{\partial z^2}$

$\Rightarrow \frac{\partial}{\partial t} \left(\nu \frac{\partial \omega}{\partial z} + Ez \omega \right) = 0$

(c) $\nu \frac{\partial \omega}{\partial z} = -Ez \omega \quad (\text{as } z \rightarrow \infty \quad \omega \rightarrow 0)$

$$\Rightarrow \omega = A \exp(-Ez^2/2\nu) \quad A = \text{constant}$$

Under example

$$\frac{du}{dz} = A \exp\left(-\frac{Ez^2}{2\nu}\right)$$

$$u = A \int_0^z \exp\left(-\frac{Es^2}{2\nu}\right) ds$$

$$s = \left(\frac{2\nu}{E}\right)^{1/2} \eta \quad u = A \left(\frac{2\nu}{E}\right)^{1/2} \int_0^{\left(\frac{E}{2\nu}\right)^{1/2} z} e^{-\eta^2} d\eta$$

$$= A \left(\frac{2\nu}{E}\right)^{1/2} \text{erf}\left(\left(\frac{E}{2\nu}\right)^{1/2} z\right)$$

$$\text{As } z \rightarrow \infty \quad \text{erf}\left(\left(\frac{E}{2\nu}\right)^{1/2} z\right) \rightarrow 1 \Rightarrow A \cdot \left(\frac{2\nu}{E}\right)^{1/2} = u_0$$

$$\Rightarrow u = u_0 \text{erf}\left(\left(\frac{E}{2\nu}\right)^{1/2} z\right)$$

$$\text{Thickness of vortex sheet} = \left(\frac{\nu}{E}\right)^{1/2}$$

(d) For long wavelengths, ~~the~~ ~~disturbance~~ $\left(\frac{1}{k} \gg \left(\frac{\nu}{E}\right)^{1/2}\right)$ the disturbance does not 'see' the viscous layer. It appears like an inviscid vortex sheet $\Rightarrow$ unstable.

[Short wavelengths could be stabilised - but this is not shown here]