

Drag on spherical droplets at vanishing Reynolds Numbers

The drag force on a stationary spherical droplet of radius a , composed of fluid with viscosity μ_2 in a fluid of viscosity μ_1 , which is flowing with uniform velocity \mathbf{U} far from the droplet, may be calculated as follows.

Outside of the droplet ($r > a$), a general solution to Stokes equations for the velocity and pressure fields are given by

$$\mathbf{u} = \mathbf{U} \left(-2Ar^2 + B\frac{a^3}{r} - C\frac{a^5}{3r^3} + D \right) + (\mathbf{U} \cdot \mathbf{x})\mathbf{x} \left(A + B\frac{a^3}{r^3} + C\frac{a^5}{r^5} \right), \quad (1)$$

$$p = \mu_1 \mathbf{U} \cdot \mathbf{x} \left(-10A + 2B\frac{a^3}{r^3} \right). \quad (2)$$

To match the far-field boundary condition, $\mathbf{u} \rightarrow \mathbf{U}$ as $|\mathbf{x}| \rightarrow \infty$, we deduce that $A = 0$ and $D = 1$.

Inside of the droplet ($r < a$), a general solution to Stokes equations for the velocity and pressure fields are given by

$$\mathbf{u} = \mathbf{U} \left(-2Er^2 + F\frac{a^3}{r} - G\frac{a^5}{3r^3} + H \right) + (\mathbf{U} \cdot \mathbf{x})\mathbf{x} \left(E + F\frac{a^3}{r^3} + G\frac{a^5}{r^5} \right), \quad (3)$$

$$p = \mu_2 \mathbf{U} \cdot \mathbf{x} \left(-10E + 2F\frac{a^3}{r^3} \right). \quad (4)$$

The velocity and pressure must be bounded at $r = 0$ and thus we deduce that $F = G = 0$.

The remaining undetermined constants are computed by applying boundary conditions at the surface of the droplet. First, because the droplet is not changing shape or volume, we demand that $\mathbf{u} \cdot \mathbf{n} = 0$ on $r = a$, where \mathbf{n} is a unit normal vector to the surface. For $r > a$ this implies that

$$2Ba^2 + \frac{2}{3}Ca^2 + 1 = 0, \quad (5)$$

while for $r < a$

$$-a^2E + H = 0. \quad (6)$$

Next we demand that the tangential component of the velocity field is continuous $r = a$, which implies that

$$-2a^2E + H = Ba^2 - \frac{1}{3}Ca^2 + 1. \quad (7)$$

Finally we enforce the continuity of the tangential component of the stress tensor at $r = a$. The normal component of the stress may not be continuous because surface tension acts on the interface to ensure that the droplet remains spherical. The stress tensor on $r = a^+$ is given by

$$\sigma_{ij} = \mu_1 \mathbf{U} \cdot \mathbf{x} \left(2C\delta_{ij} - \frac{x_i x_j}{a^2} (6B + 10C) \right) + \mu_1 U_i x_j 2C + \mu_1 U_j x_i 2C, \quad (8)$$

while the stress tensor at $r = a^-$ is given by

$$\sigma_{ij} = \mu_2 12E \mathbf{U} \cdot \mathbf{x} \delta_{ij} - \mu_2 U_i x_j 3E - \mu_2 U_j x_i 3E. \quad (9)$$

Equating the tangential components of the stress tensor at $r = a$ then yields

$$\mu_1 2C = -3E\mu_2. \quad (10)$$

We may therefore determine the unknown constants

$$E = -\frac{\lambda}{2(1+\lambda)a^2}, \quad B = -\frac{1}{2a^2} - \frac{1}{4(1+\lambda)a^2}, \quad C = \frac{3}{4(1+\lambda)a^2} \quad \text{and} \quad H = -\frac{1}{2(1+\lambda)}, \quad (11)$$

where $\lambda = \mu_1/\mu_2$.

The drag on the droplet, \mathbf{F} , is evaluated by computing the surface stress $\sigma_{ij}n_j$ integrated over the surface $r = a$. This gives

$$F_i = \frac{\mu_1 U_k}{a} \int_{r=a} -6(B+C)x_k x_i + 2a^2 C \delta_{ik} \, dS \quad (12)$$

$$= \frac{\mu_1 U_k}{a} \left(\frac{4\pi a^4}{3} \delta_{ik} \frac{6\lambda}{2a^2(1+\lambda)} + 4\pi a^4 \delta_{ik} \frac{6}{4a^2(1+\lambda)} \right) \quad (13)$$

$$= \mu_1 U_i a \pi \frac{(4\lambda + 6)}{1 + \lambda}. \quad (14)$$

Note that when $\lambda \rightarrow \infty$, $F_i \rightarrow 4\pi a \mu_1 U_i$, which recovers the result for viscous flow past a spherical droplet of inviscid fluid. Further note that when $\lambda \rightarrow 0$, $F_i \rightarrow 6\pi a \mu_1 U_i$, which recovers the result for flow past a solid spherical particle.